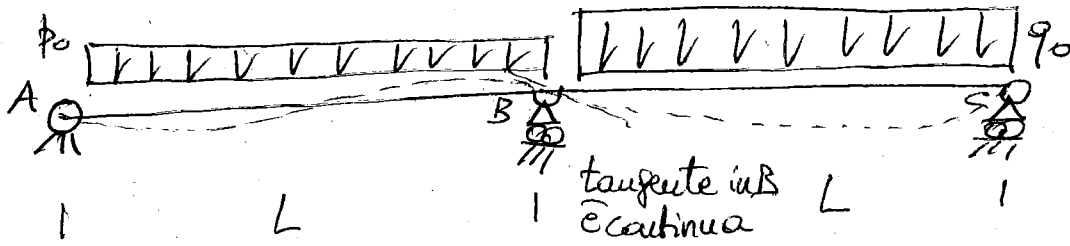
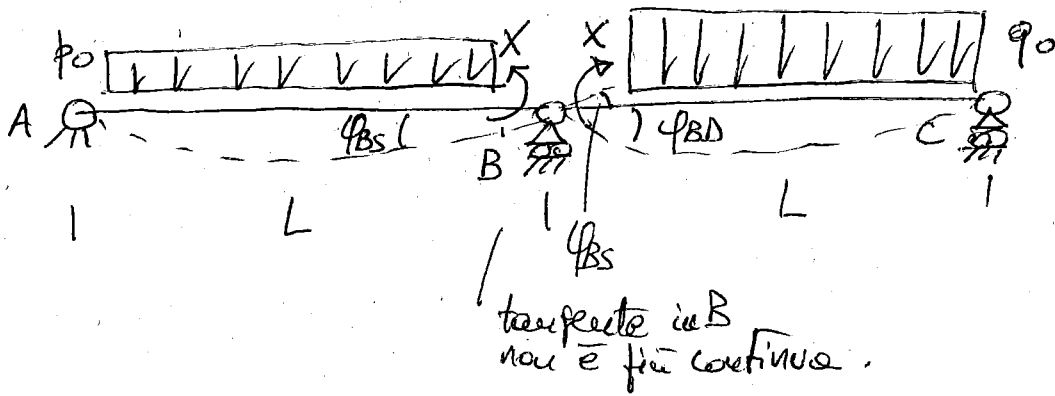


# Principio dei lavori virtuali per travi iperstatiche

Applicazione al caso di travi continue.

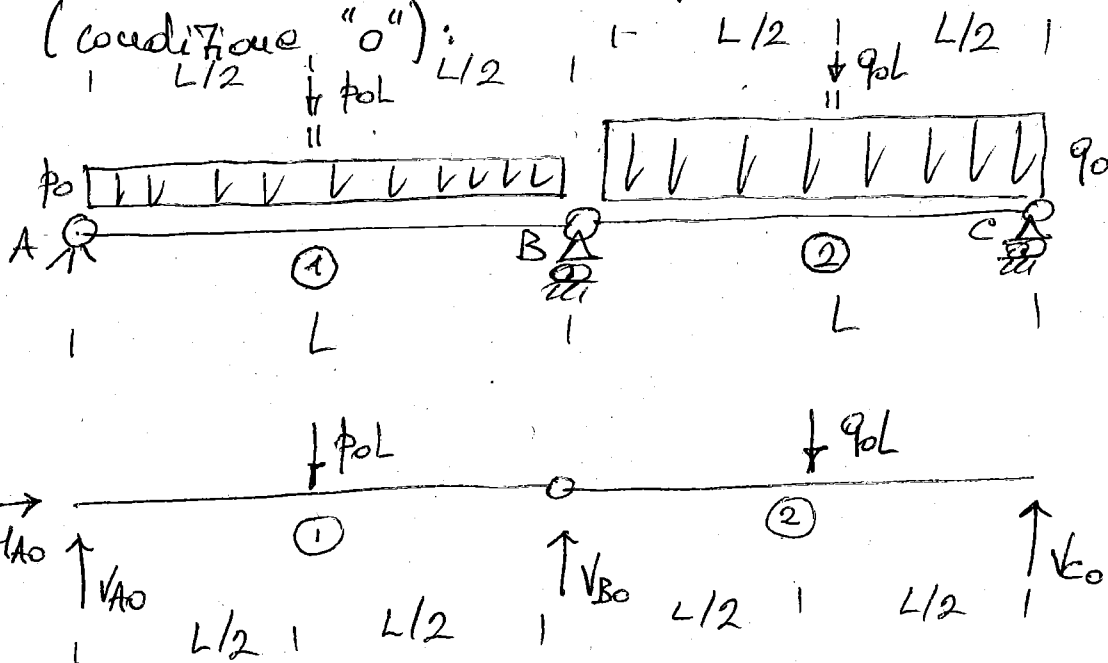


Struttura iperstatica:  
 $\Delta \varphi_B = 0$



Struttura iperstatica:  
 $\Delta \varphi_B = \varphi_{BS} + \varphi_{BD} \neq 0$

A) Struttura iperstatica soggetta a sole azioni esterne (condizione "0"):



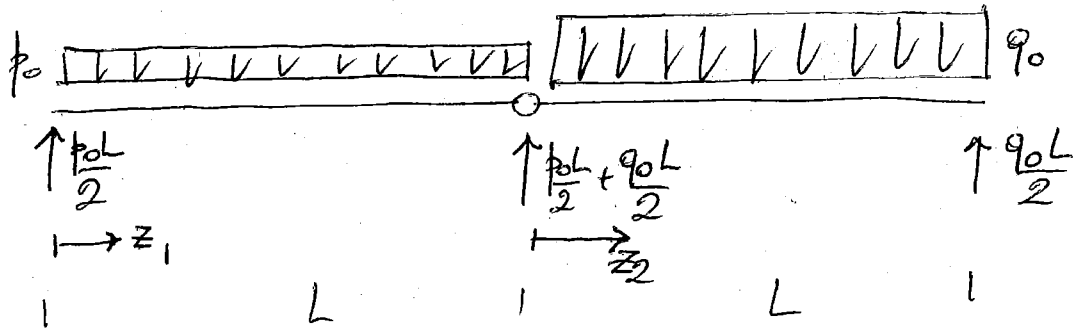
$$\rightarrow R_x = 0 \quad H_{A0} = 0$$

$$\uparrow R_y = 0 \quad V_{A0} + V_{B0} + V_{C0} - P_0 L - q_0 L = 0 \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{eq. cardinali}$$

$$5 M_{z(A)} = 0 \quad - \frac{P_0 L^2}{2} + V_{B0} L - \frac{3}{2} q_0 L^2 + V_{C0} \cdot 2L = 0$$

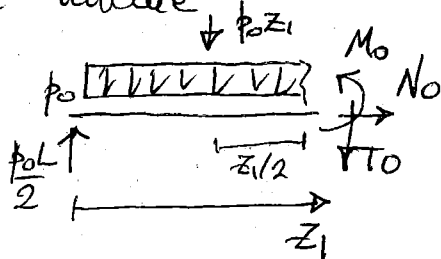
$$5 M_{z(B)} = 0 \quad - \frac{q_0 L^2}{2} + V_{C0} L = 0 \quad \text{eq. ausiliaria}$$

segue:  $H_{A0} = 0$ ;  $V_{C0} = \frac{q_0 L}{2}$ ;  $V_{B0} = \frac{P_0 L}{2} + \frac{q_0 L}{2}$ ;  $V_{A0} = \frac{P_0 L}{2}$



Azioni interne

①

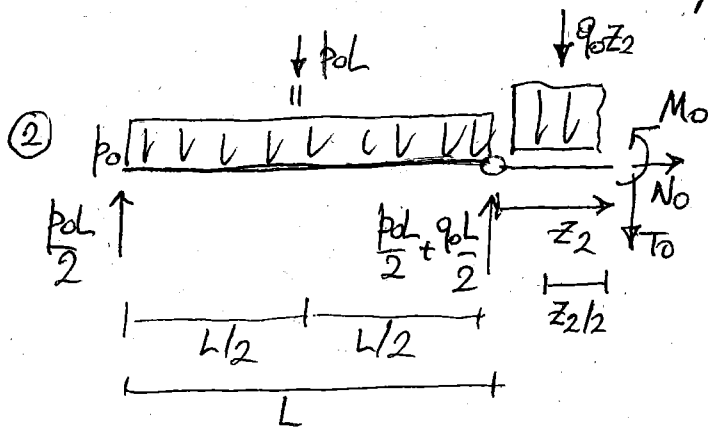
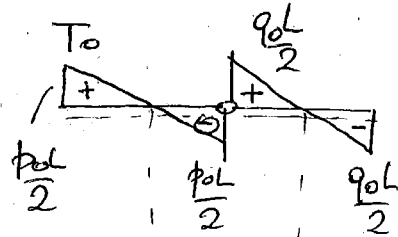
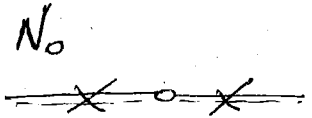


A → B  
0 ≤ z<sub>1</sub> < L

$$N_0(z_1) = 0$$

$$T_0(z_1) = \frac{p_0 L}{2} - p_0 z_1$$

$$M_0(z_1) = \frac{p_0 L}{2} z_1 - \frac{p_0 z_1^2}{2}$$

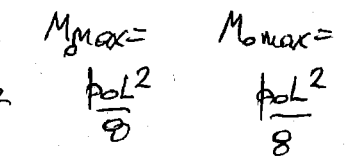
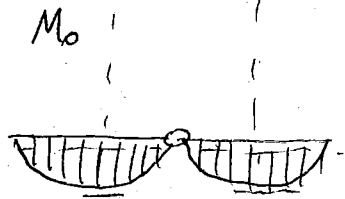


B → C  
0 < z<sub>2</sub> ≤ L

$$N_0(z_2) = 0$$

$$T_0(z_2) = \frac{q_0 L}{2} - q_0 z_2$$

$$M_0(z_2) = \frac{q_0 L z_2}{2} - \frac{q_0 z_2^2}{2}$$



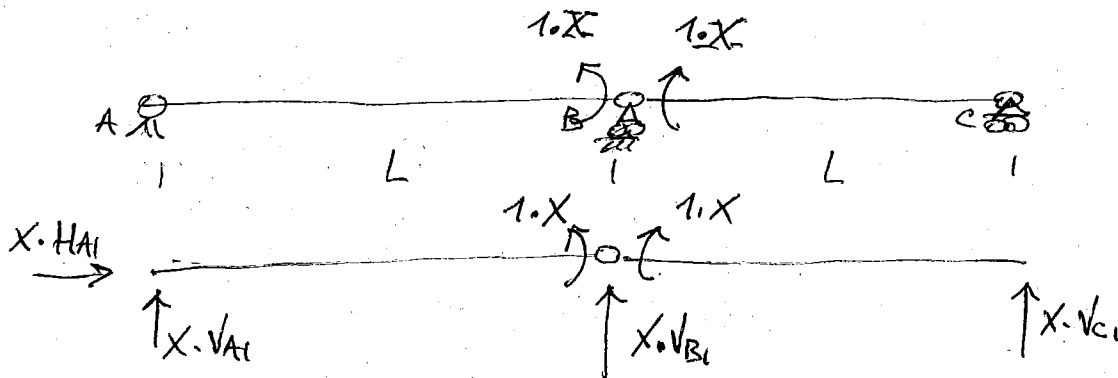
infatti  $\sum M_{(z_2)} = 0$

$$-\frac{p_0 L}{2} \cdot (L + z_2) + p_0 L \left(\frac{L}{2} + z_2\right) - \left(\frac{p_0 L}{2} + \frac{q_0 L}{2}\right) z_2 + q_0 \frac{z_2^2}{2} + M_0(z_2) = 0$$

$$M_0(z_2) = \frac{p_0 L^2}{2} + \frac{p_0 L}{2} z_2 - \frac{p_0 L^2}{2} - \frac{p_0 L}{2} z_2 + \frac{p_0 L}{2} z_2 + \frac{q_0 L}{2} z_2 - q_0 \frac{z_2^2}{2} = \frac{q_0 L}{2} z_2 - \frac{q_0 z_2^2}{2}$$

B) Struttura reso isostatica soggetta alle sole azioni delle ipostati

X = 1 · X (condizione "1" · X)



→ R<sub>x</sub> = 0    X · H<sub>A1</sub> = 0

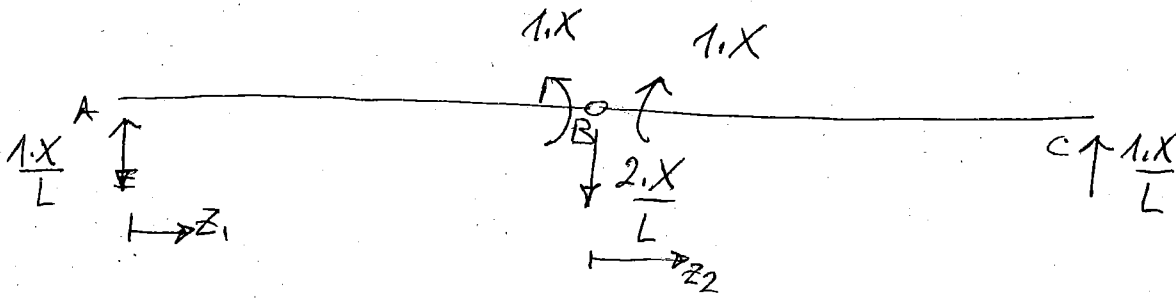
↑ R<sub>y</sub> = 0    X · V<sub>A1</sub> + X · V<sub>B1</sub> + X · V<sub>C1</sub> = 0

∑ M<sub>ZCA</sub> = 0    X · V<sub>B1</sub> · L + X · V<sub>C1</sub> · 2L = 0

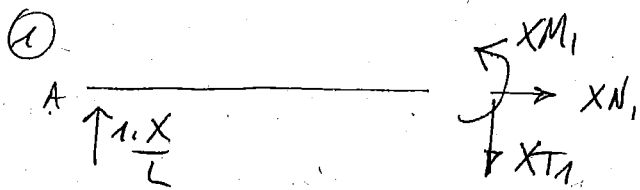
eq. cardinali

5.  $M_Z^{(2)} = 0 - 1 \cdot X + X \cdot \sqrt{L} = 0$  eq. coefficient

ne segue:  $X_{HA1} = 0$ ;  $X_{V_{C1}} = \frac{1 \cdot X}{L}$ ;  $X_{V_{B1}} = -2 \frac{1 \cdot X}{L}$ ;  $X_{V_{A1}} = \frac{1 \cdot X}{L}$



Azioni interne:



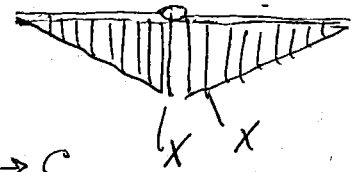
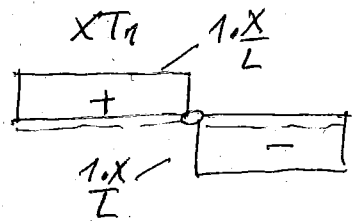
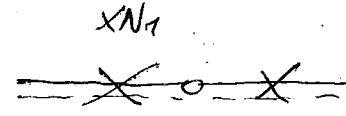
A → B

$0 \leq z_1 < L$

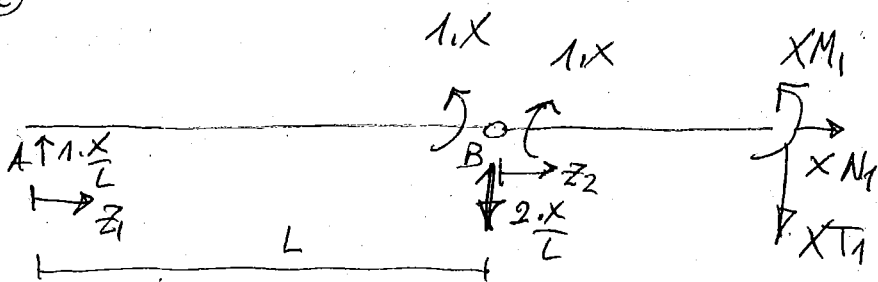
$X_{N1}(z_1) = 0$

$X_{T1}(z_1) = \frac{1 \cdot X}{L}$

$X_{M1}(z_1) = \frac{1 \cdot X}{L} z_1$



②



B → C

$0 \leq z_2 \leq L$

$X_{N1}(z_2) = 0$

$X_{T1}(z_2) = -\frac{1 \cdot X}{L}$

$X_{M1}(z_2) = X \left(1 - \frac{z_2}{L}\right)$

infatti  $\sum M_{(z_2)} = 0 - \frac{1 \cdot X}{L} (L + z_2) + 1 \cdot X - 1 \cdot X + \frac{2 \cdot X}{L} z_2 + X_{M1}(z_2) = 0$

$X_{M1}(z_2) = \frac{1 \cdot X}{L} L + \frac{1 \cdot X}{L} z_2 - 1 \cdot X + 1 \cdot X - \frac{2 \cdot X}{L} z_2 = 1 \cdot X - \frac{1 \cdot X}{L} z_2$

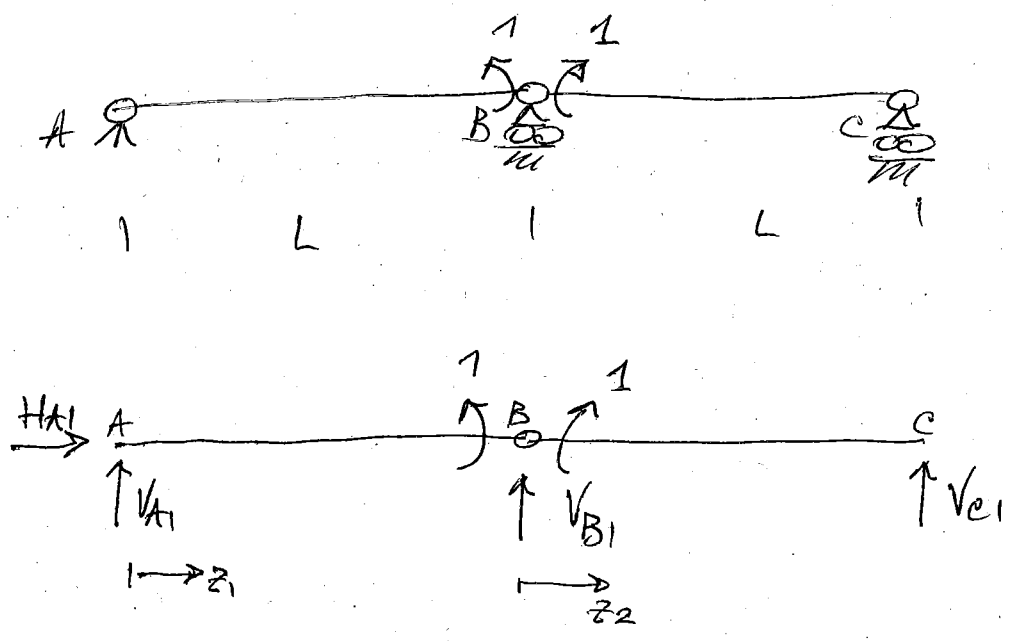
c) Sistema cedé: spostamenti e deformazioni complessivi

$\epsilon = \frac{N_0 + X_{N1}}{EA} = 0 \quad \forall z_1, \forall z_2$

$\gamma = \frac{T_0 + X_{T1}}{GA_T} = \begin{cases} \frac{p_0 L / 2 - p_0 z_1 + X_{T1}}{GA_T} & A \rightarrow B \\ \frac{q_0 L / 2 - q_0 z_2 + X_{T1}}{GA_T} & B \rightarrow C \end{cases}$

$$X = \frac{M_0 + XM_1}{EI} = \begin{cases} \frac{p_0 L z_1 - p_0 \frac{z_1^2}{2} + X \frac{z_1}{L}}{EI} & A \rightarrow B \\ & 0 \leq z_1 < L \\ \frac{q_0 L z_2 - q_0 \frac{z_2^2}{2} + X(1 - \frac{z_2}{L})}{EI} & B \rightarrow C \\ & 0 < z_2 \leq L \end{cases}$$

D) Sistema ausiliario: forze e spostamenti in equilibrio

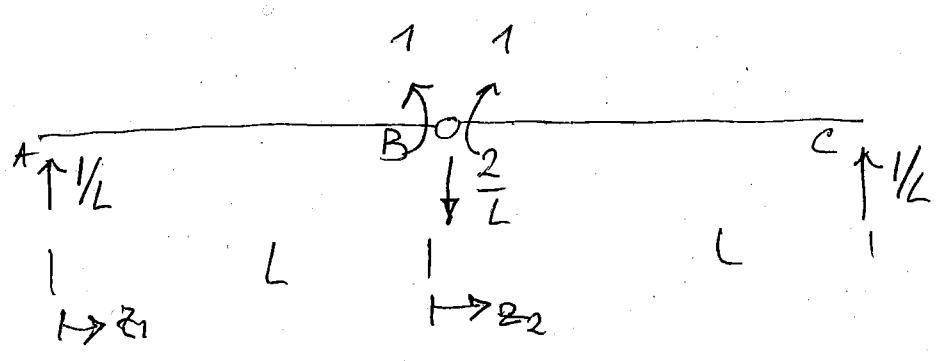


NB: Le 2 coppie applicate coefficiente unitario rispettivamente per \$P\_B\$ e \$P\_D\$

Nota: È EQUIVALENTE alla struttura reale isostatica soggetta alla sola azione dell'ipostatica quando si sceglie \$X=1\$.

Pertanto:

$$H_{A1} = 0 ; V_{A1} = \frac{1}{L} ; V_{B1} = -\frac{2}{L} ; V_{C1} = \frac{1}{L}$$



e analoga per le azioni interne p. 4/7

$$\left. \begin{aligned} N_1(z_1) &= 0 \\ T_1(z_1) &= \frac{1}{L} \\ M_1(z_1) &= \frac{1}{L} z_1 \end{aligned} \right\} \begin{aligned} A \rightarrow B \\ 0 \leq z_1 < L \end{aligned}$$

$$\left. \begin{aligned} N_1(z_2) &= 0 \\ T_2(z_2) &= -\frac{1}{L} \\ M_1(z_2) &= 1 \left(1 - \frac{z_2}{L}\right) \end{aligned} \right\} \begin{aligned} B \rightarrow C \\ 0 \leq z_2 < L \end{aligned}$$

E) APPLICAZIONE DEL P.L.V. (trascurando deformazione a taglio)

$$L_e = 1 \cdot \varphi_{BS} + 1 \cdot \varphi_{BD} = 1 \cdot \Delta \varphi_B = 0$$

↑  $\Delta \varphi_B = 0$  per compattezza.

$$L_i = \int_0^L N_1 \cdot \varepsilon dz_1 + \int_0^L N_2 \cdot \varepsilon dz_2 + \int_0^L M_1 \chi dz_1 + \int_0^L M_2 \chi dz_2$$

$$L_i = \int_0^L 1 \cdot \frac{z_1}{L} \left( \frac{p_0 L z_1 - p_0 z_1^2}{2 E I} + \chi \frac{z_1}{L} \right) dz_1 + \int_0^L 1 \cdot \left(1 - \frac{z_2}{L}\right) \left[ \frac{q_0 L z_2 - q_0 \frac{z_2^2}{2} + \chi \left(1 - \frac{z_2}{L}\right)}{E I} \right] dz_2$$

$$L_e = L_i \Rightarrow L_i = 0 \quad \text{ovvero} \quad C_{10} + \chi C_{11} = 0$$

$$L_i = \int_0^L 1 \cdot \frac{z_1}{L} \frac{p_0 L z_1 - p_0 z_1^2}{2 E I} dz_1 + \chi \int_0^L 1 \cdot \frac{z_1}{L} \frac{z_1}{L} dz_1 +$$

$$+ \int_0^L 1 \cdot \left(1 - \frac{z_2}{L}\right) \frac{q_0 L z_2 - q_0 \frac{z_2^2}{2}}{E I} dz_2 + \chi \int_0^L 1 \cdot \left(1 - \frac{z_2}{L}\right) \frac{\left(1 - \frac{z_2}{L}\right)}{E I} dz_2$$

$$L_i = \left\{ \int_0^L \frac{p_0 L z_1^2 - p_0 z_1^3}{2 L E I} dz_1 + \int_0^L \frac{q_0 L z_2 - \frac{q_0 z_2^2}{2} - \frac{q_0 z_2^2}{2} + \frac{q_0 z_2^3}{2 L}}{E I} dz_2 \right\} +$$

$$+ \chi \left\{ \int_0^L \frac{z_1^2}{L^2 E I} dz_1 + \int_0^L \frac{\left(1 - \frac{z_2}{L}\right)^2}{E I} dz_2 \right\}$$

$C_{10}$        $C_{11}$

$$C_{10} = \frac{1}{EI} \left\{ \int_0^L \left( \frac{p_0 z_1^2}{2} - \frac{p_0 z_1^3}{2L} \right) dz_1 + \int_0^L \left( \frac{q_0 L}{2} z_2 - q_0 z_2^2 + \frac{q_0 z_2^3}{2L} \right) dz_2 \right\}$$

$$C_{10} = \frac{1}{EI} \left[ \frac{p_0 z_1^3}{6} - \frac{p_0 z_1^4}{8L} \right]_0^L + \frac{1}{EI} \left[ \frac{q_0 L z_2^2}{4} - \frac{q_0 z_2^3}{3} + \frac{q_0 z_2^4}{8L} \right]_0^L$$

$$C_{10} = \frac{p_0 L^3}{6EI} - \frac{p_0 L^3}{8EI} + \frac{q_0 L^3}{4EI} - \frac{q_0 L^3}{3EI} + \frac{q_0 L^3}{8EI} = \frac{(4-3)p_0 L^3}{24EI} + \frac{(6-8+3)q_0 L^3}{24EI}$$

$$C_{10} = \frac{p_0 L^3}{24EI} + \frac{q_0 L^3}{24EI}$$

$$C_{11} = \frac{1}{EI} \left\{ \int_0^L \frac{z_1^2}{L^2} dz_1 + \int_0^L \left( \frac{L-z_2}{L} \right)^2 dz_2 \right\}$$

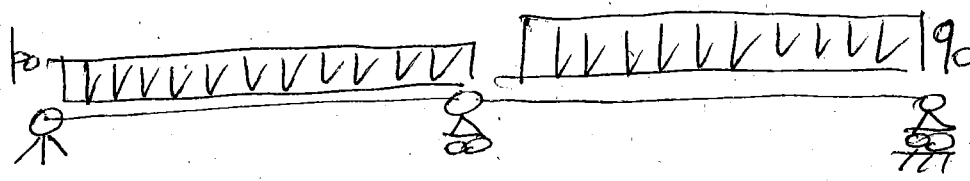
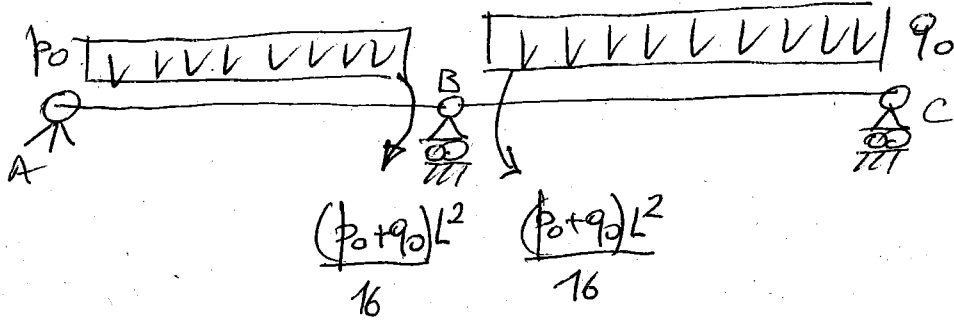
$$C_{11} = \frac{1}{EI} \left[ \frac{z_1^3}{3L^2} \right]_0^L + \frac{1}{EI} \left[ \left( \frac{1-z_2}{L} \right)^3 \cdot \left( -\frac{L}{3} \right) \right]_0^L$$

$$C_{11} = \frac{L}{3EI} + \frac{L}{3EI} = \frac{2L}{3EI}$$

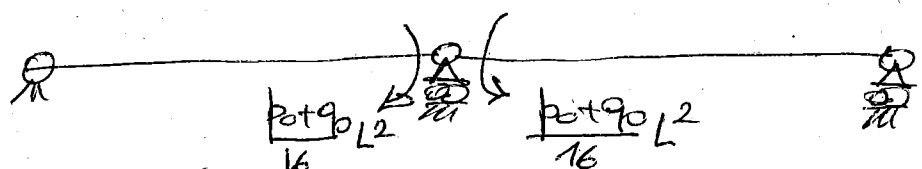
$$C_{10} + X C_{11} = 0 \Rightarrow X = - \frac{C_{10}}{C_{11}} = - \frac{\frac{p_0 L^3}{24EI} + \frac{q_0 L^3}{24EI}}{\frac{2L}{3EI}}$$

ovvero  $X = - \frac{p_0 L^2}{16} - \frac{q_0 L^2}{16}$

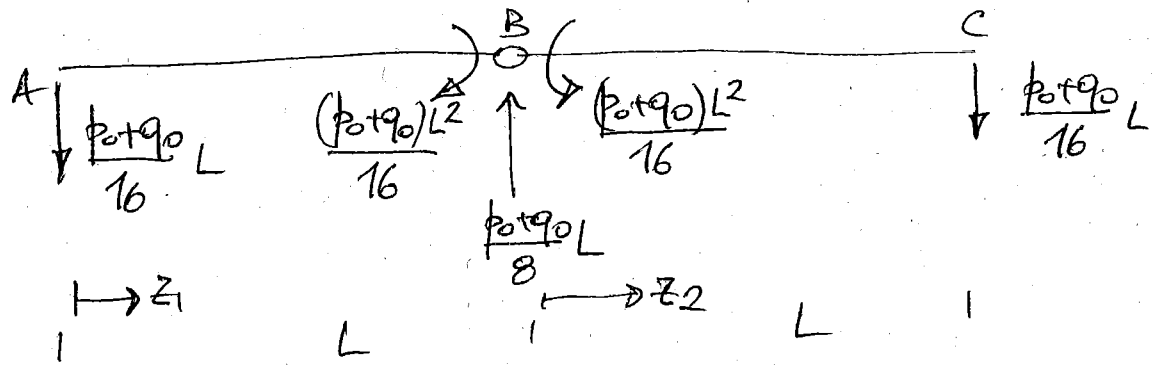
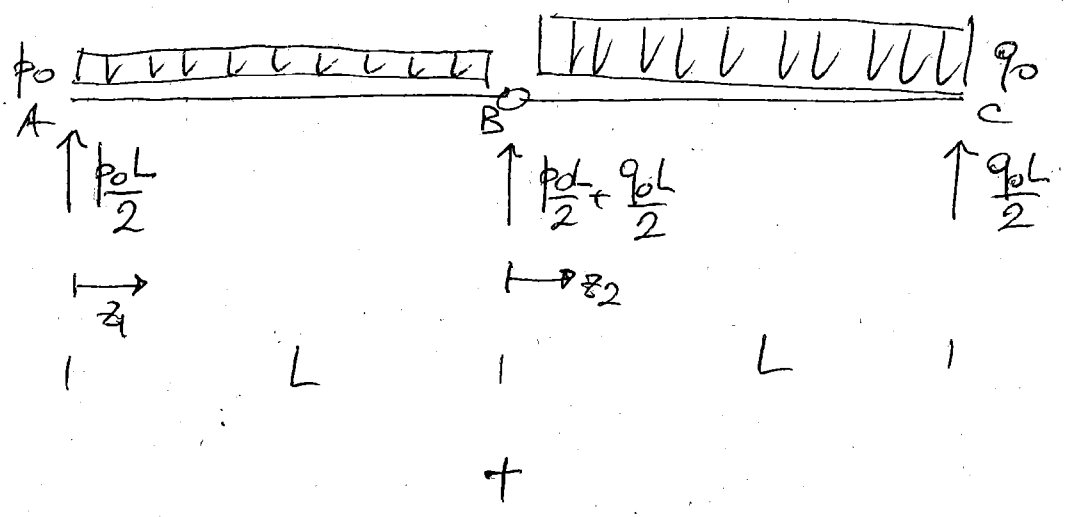
F) SOSTITUZIONE DEL VALORE DELL'IPERSTATICA



(STATO "0")



(STATO "1.0X")



Perfando

$$N = N_0 - \left(\frac{p_0 + q_0}{16}\right) L^2 N_1 = \begin{cases} 0 & A \rightarrow B \\ 0 & B \rightarrow C \end{cases}$$

$0 \leq z_1 < L$   
 $0 \leq z_2 \leq L$

$$T = T_0 - \left(\frac{p_0 + q_0}{16}\right) L^2 T_1 = \begin{cases} \frac{7}{16} p_0 L - p_0 z_1 - \frac{1}{16} q_0 L & A \rightarrow B \\ \frac{9}{16} q_0 L - q_0 z_2 + \frac{1}{16} p_0 L & B \rightarrow C \end{cases}$$

$0 \leq z_1 < L$   
 $0 \leq z_2 \leq L$

$$M = M_0 - \left(\frac{p_0 + q_0}{16}\right) L^2 M_1 = \begin{cases} \frac{7}{16} p_0 L z_1 - \frac{p_0 z_1^2}{2} - \frac{1}{16} q_0 L z_1 & A \rightarrow B \\ -\frac{q_0 L^2}{16} + \frac{9}{16} q_0 L z_2 - \frac{q_0 z_2^2}{2} - \frac{p_0 L^2}{16} + \frac{p_0 L z_2}{16} & B \rightarrow C \end{cases}$$

$0 \leq z_1 < L$   
 $0 \leq z_2 \leq L$

