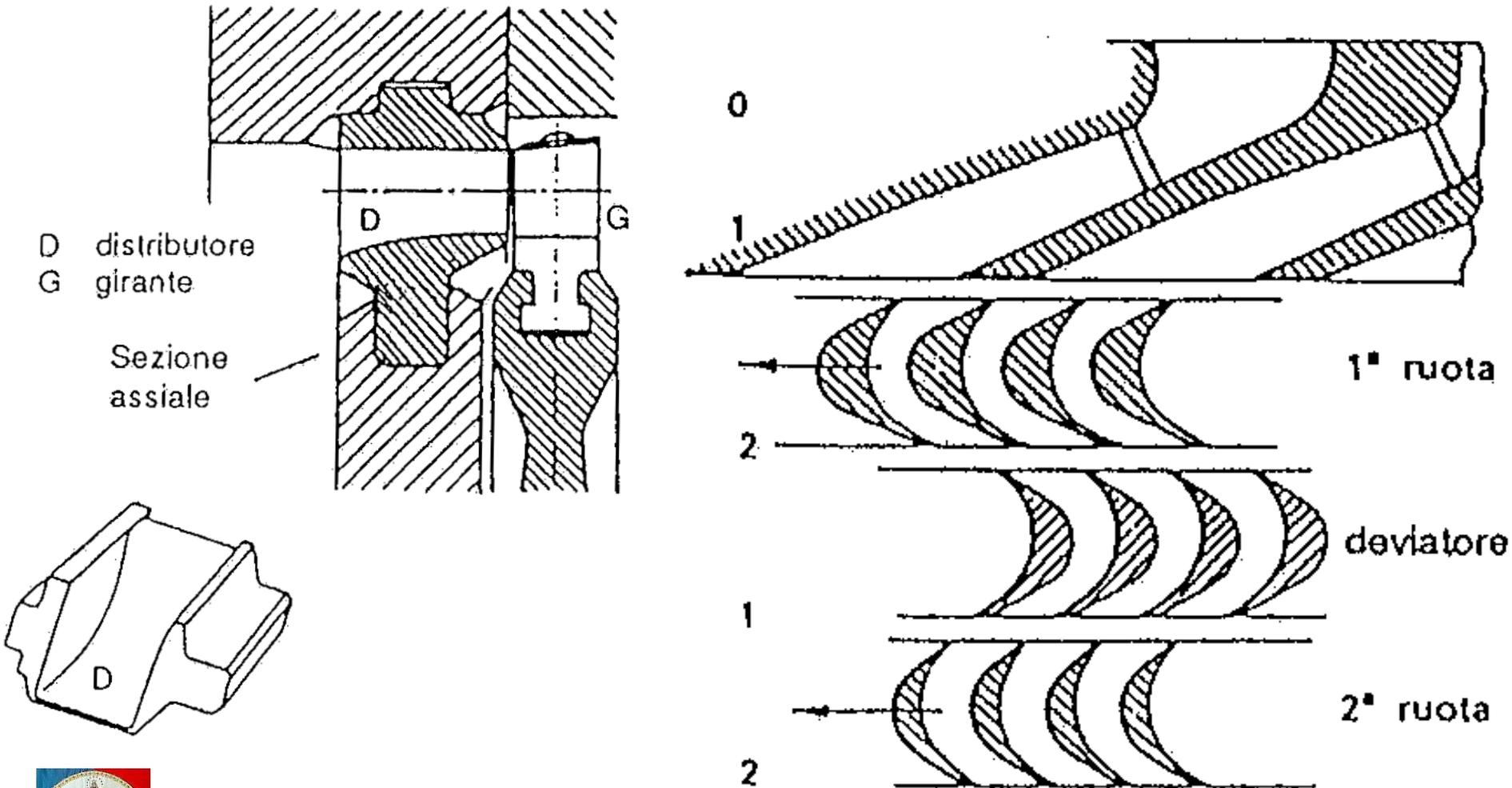
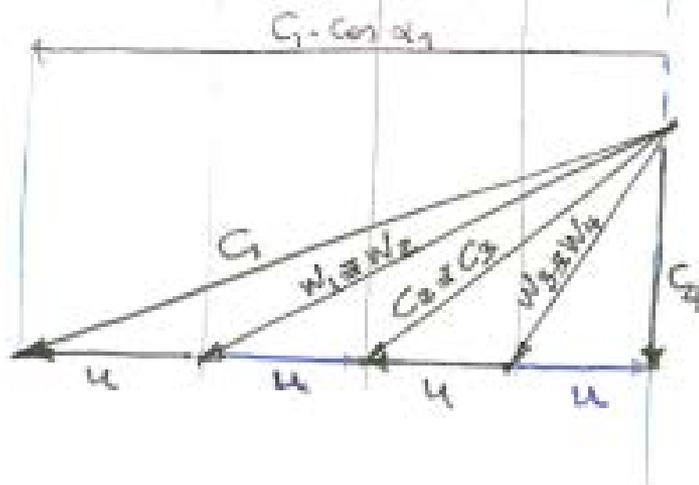
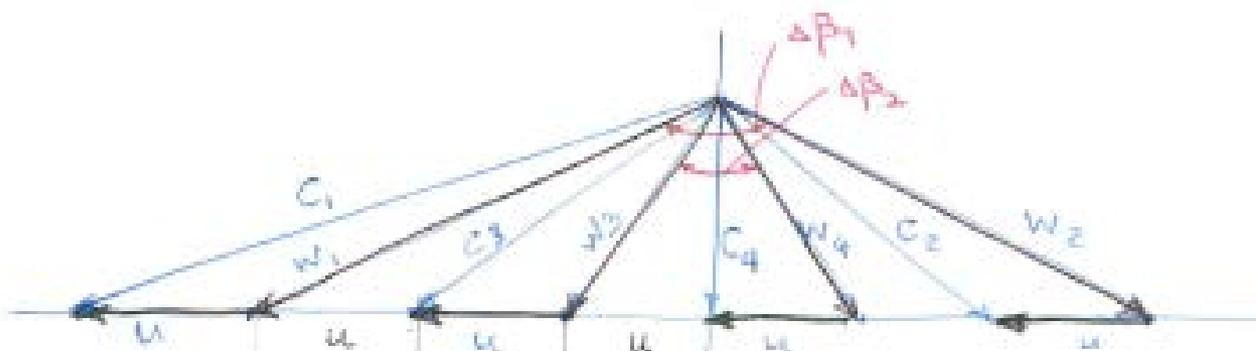


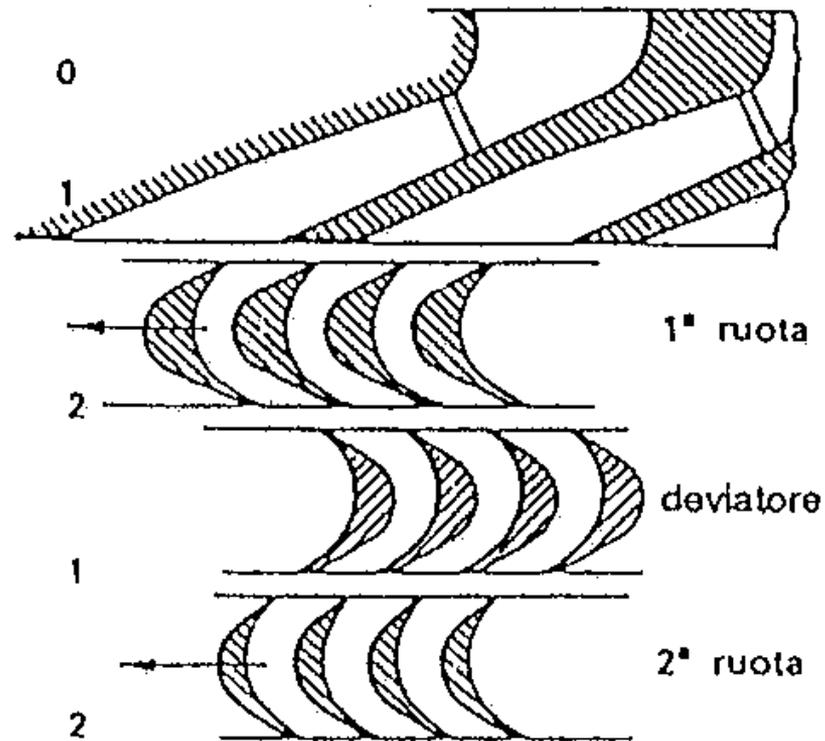
Turbina ad azione a salti di velocità: Turbina Curtis



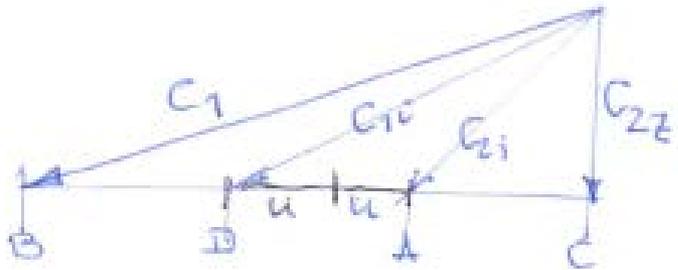
MACCHINE A FLUIDO



$$C_1 \cos \alpha_1 = 2u \cdot z$$



Ripartizione della potenza nella turbina Curtis



$$P = \frac{C_1^2 C_2^3}{2} + \frac{u_1^2 u_2^2}{2} - \frac{w_1^2 w_2^3}{2}$$

$$P_i = \frac{C_{1i}^2 - C_{2i}^2}{2} = \frac{C_{1i}^2 - C_{2E}^2}{2} - \frac{C_{2i}^2 - C_{2E}^2}{2}$$

$$C_{1i}^2 - C_{2E}^2 = \overline{DC}^2 \quad C_{2i}^2 - C_{2E}^2 = \overline{AC}^2$$

$$P_i = \frac{1}{2} (\overline{DC}^2 - \overline{AC}^2) = \frac{1}{2} \left\{ \left[2u(\varepsilon - i + 1) \right]^2 - \left[2u(\varepsilon - i) \right]^2 \right\} = 2u^2 (2\varepsilon - 2i + 1)$$

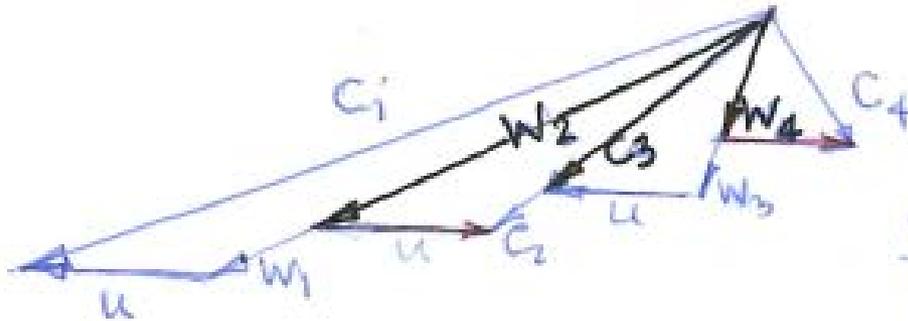
$$P_{tot} = \frac{C_1^2 - C_{2E}^2}{2} = \frac{\overline{BC}^2}{2} = \frac{(2u\varepsilon)^2}{2} = 2u^2 \varepsilon^2$$

$$\frac{P_i}{P_{tot}} = \frac{2u^2 (2\varepsilon - 2i + 1)}{2u^2 \varepsilon^2} = \frac{2\varepsilon - 2i + 1}{\varepsilon^2}$$

Al crescere di ε , la potenza captata dagli ultimi stadi diminuisce in maniera minima



MACCHINE A FLUIDO



Triangolo di velocità nel caso reale

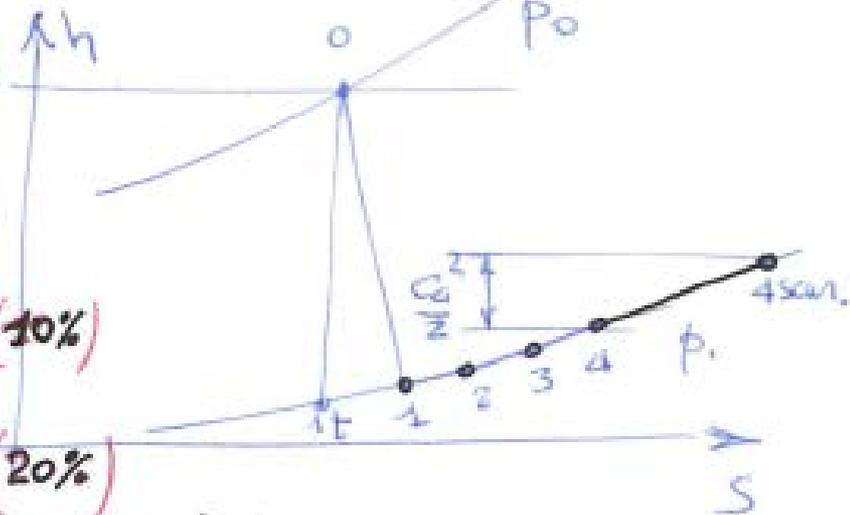
Rendimento isentropico

$$\text{statore } h_1 - h_{1t} = \frac{C_{1t}^2 - C_1^2}{2} = \frac{C_{1t}^2}{2} (1 - \varphi^2) \quad (10\%)$$

$$\text{rot. 1 } h_2 - h_1 = \frac{W_1^2 - W_2^2}{2} = \frac{W_1^2}{2} (1 - \varphi_1^2) \quad (20\%)$$

$$\text{dev. } h_3 - h_2 = \frac{C_2^2 - C_3^2}{2} = \frac{C_2^2}{2} (1 - \varphi_D^2) \quad (7\%)$$

$$\text{rot. 2 } h_4 - h_3 = \frac{W_3^2 - W_4^2}{2} = \frac{W_3^2}{2} (1 - \varphi_2^2) \quad (4\%)$$



$\varphi_2 > \varphi_D > \varphi_1$ perché
 $\Delta\beta_2 < \Delta\beta_D < \Delta\beta_1$



Regolazione per parzializzazione

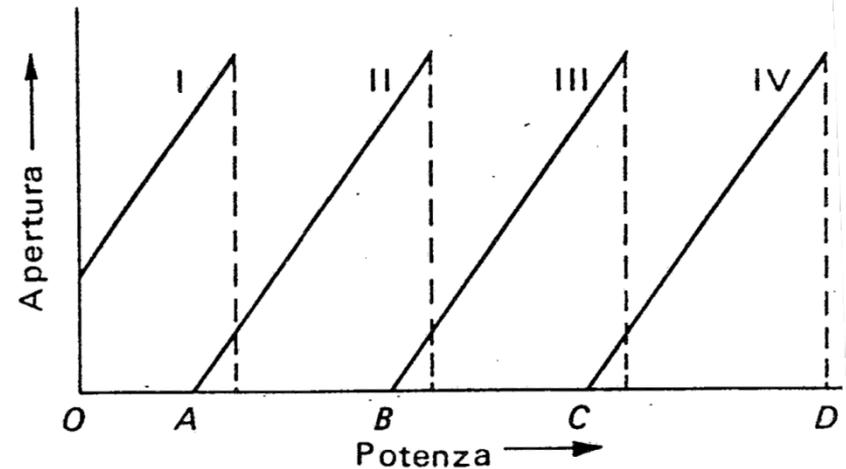
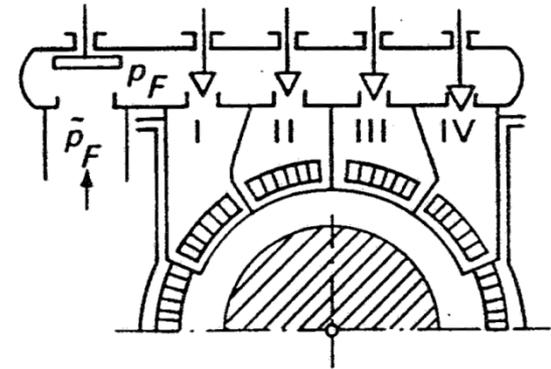
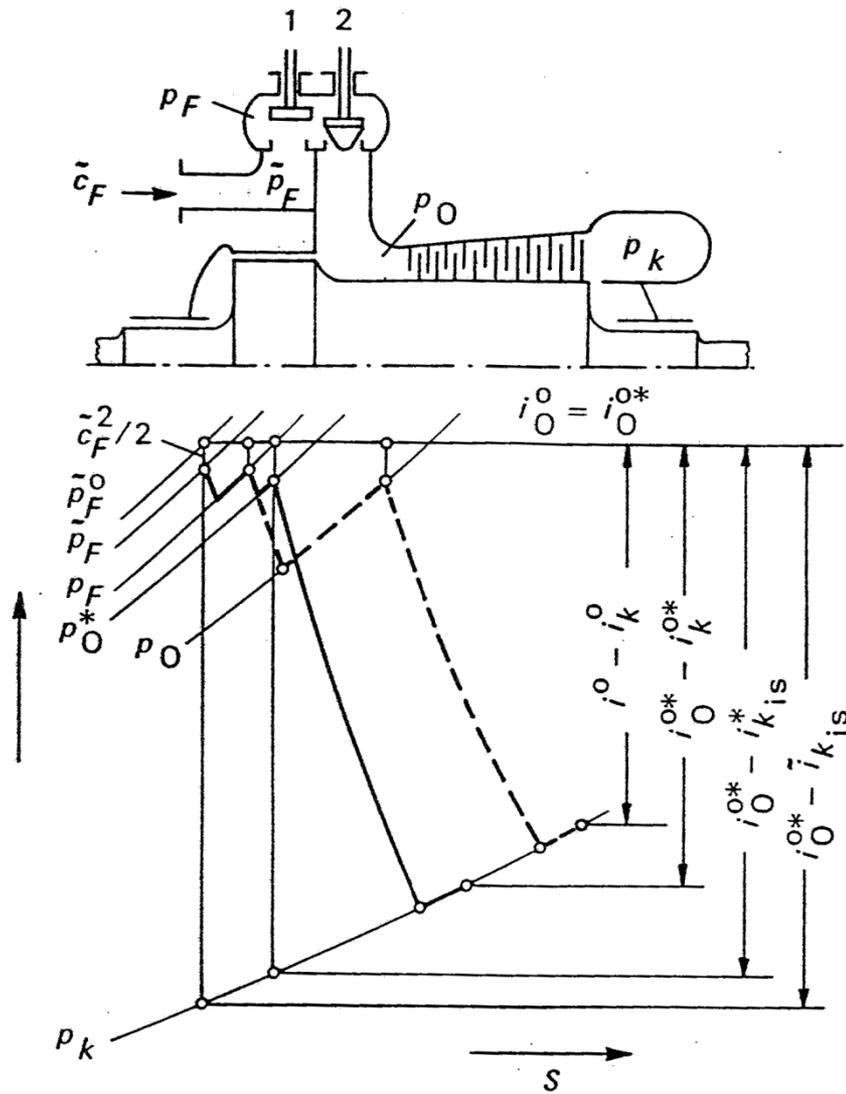


Fig. 221

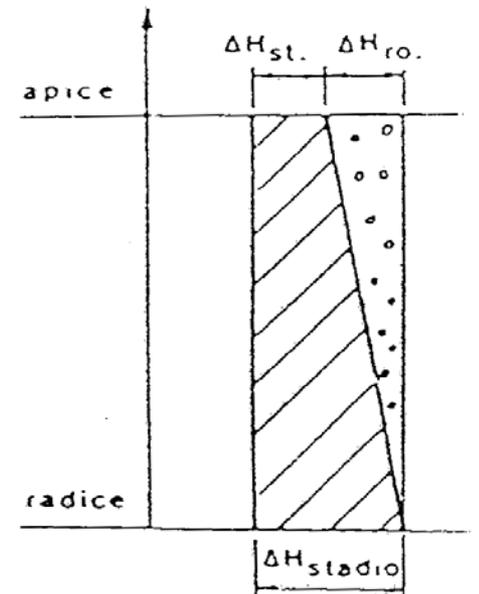
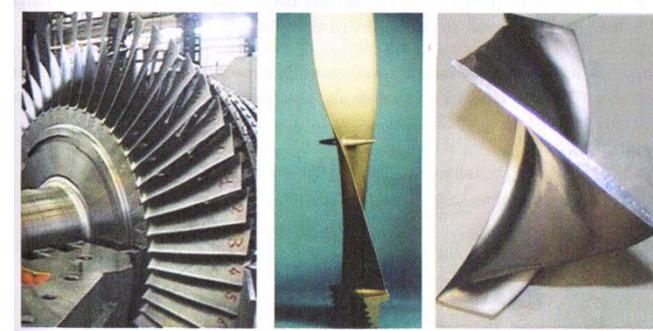
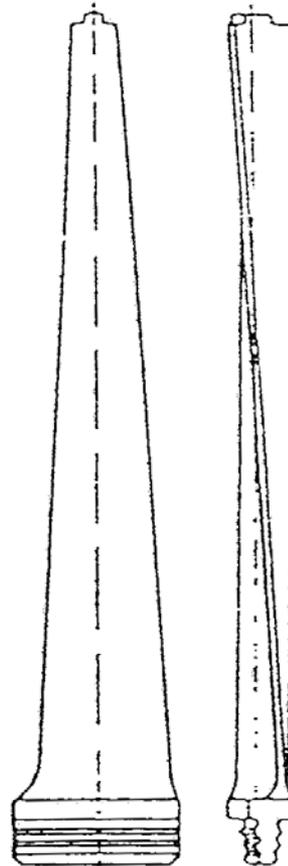
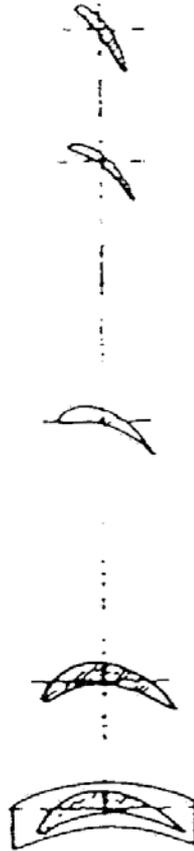
1 Valvola di sicurezza;
I, II, III, IV Valvole di parzializzazione.

Regolazione per laminazione

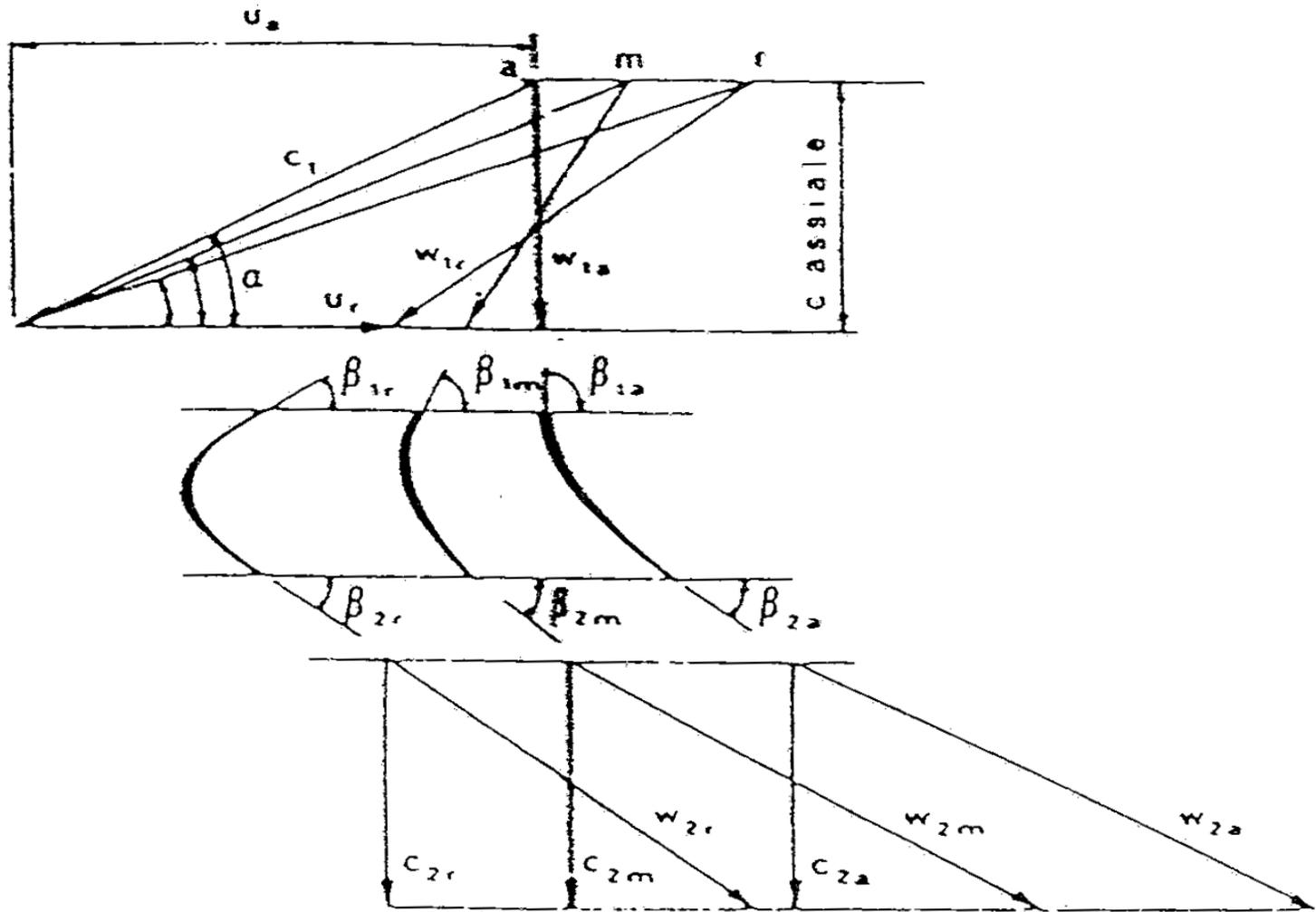


Svergolatura della pala rotorica

Pala statorica *Pala rotorica*

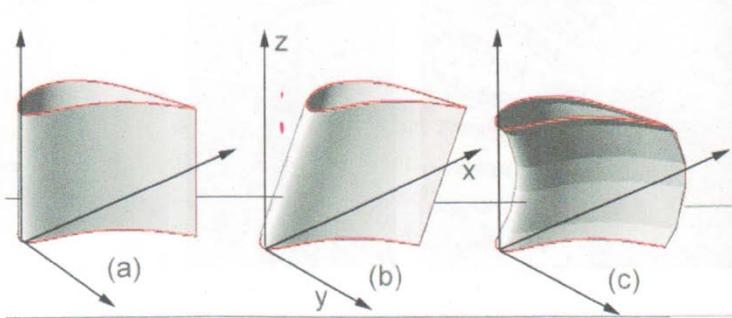


Svergolatura della pala rotorica



MACCHINE A FLUIDO

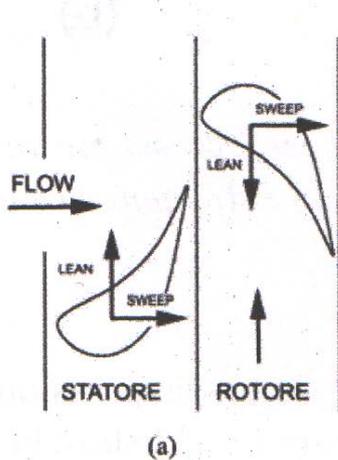
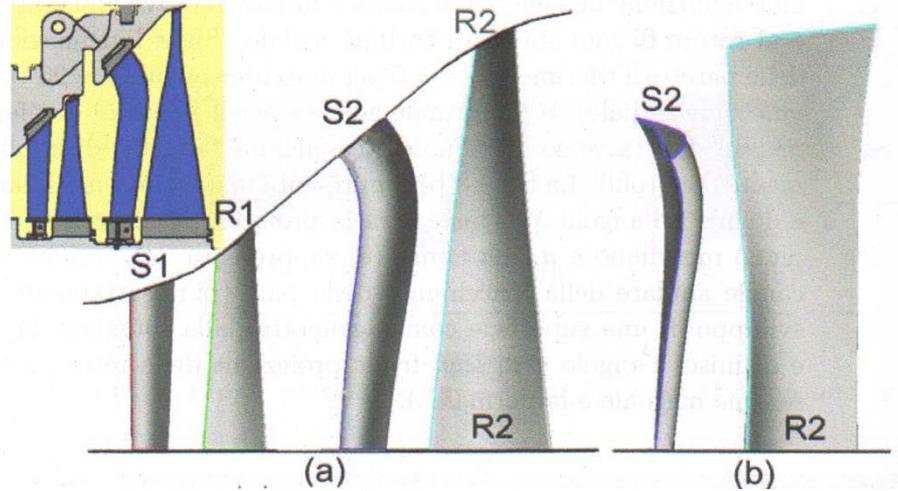
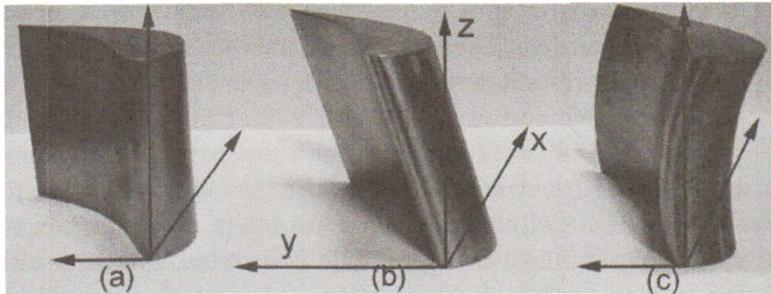
Pale con sezioni uguali ma impilate lungo linee generiche



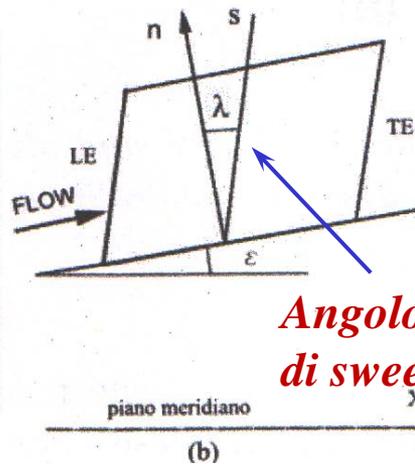
Prismatica

Leaned

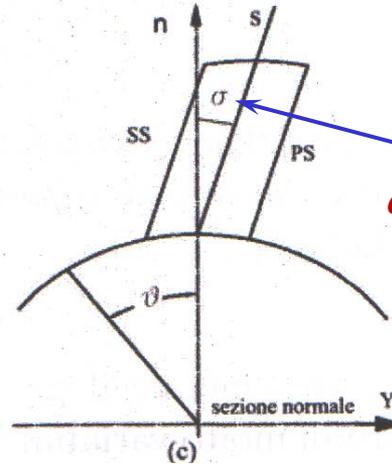
Bowed



(a)



(b)



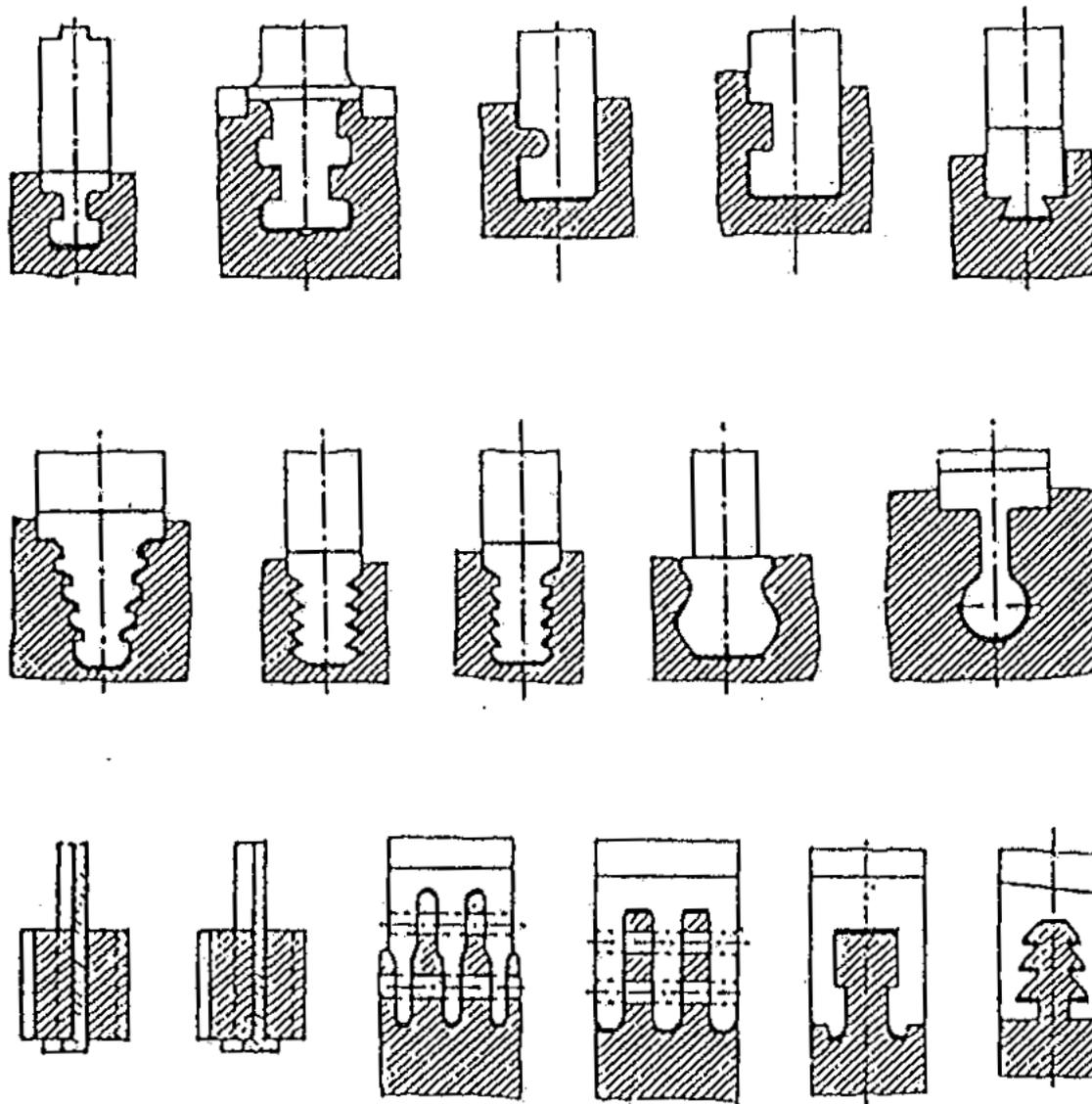
(c)

angolo di lean

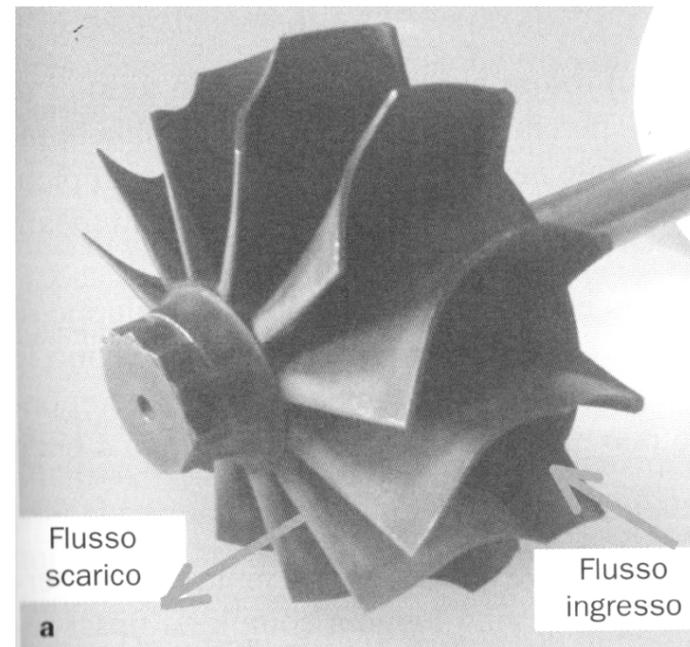
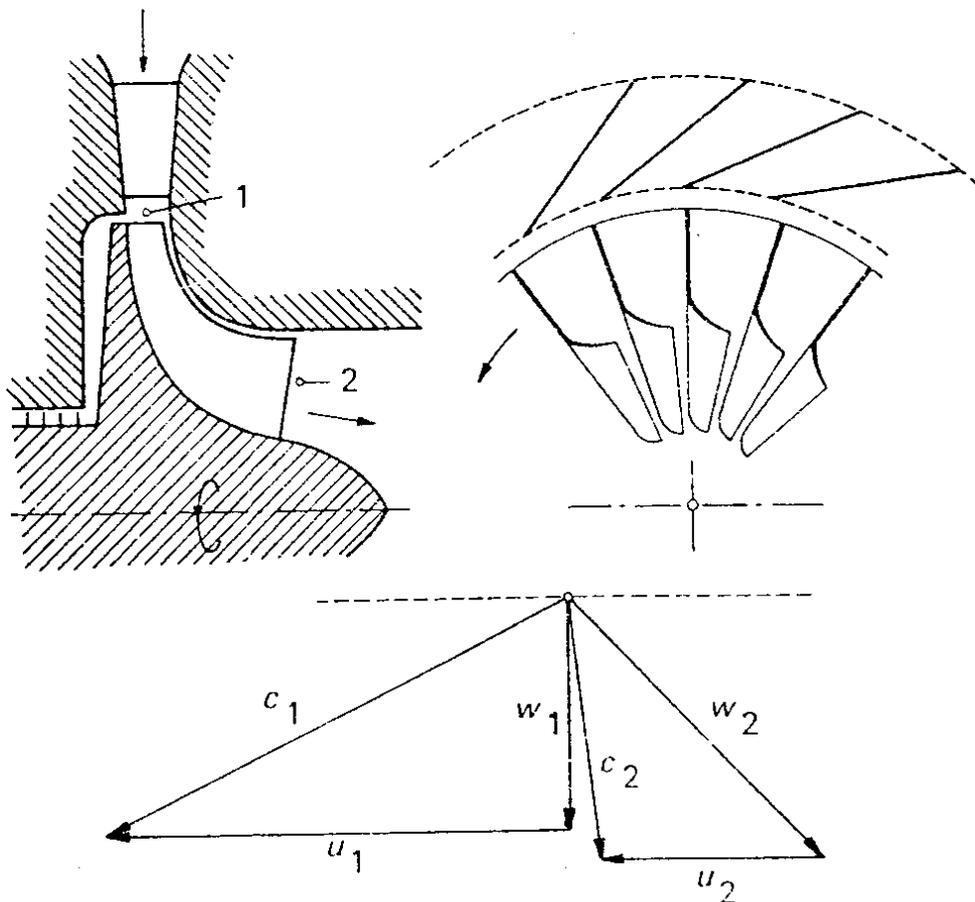
Angolo di sweep



Attacchi delle palette di macchine assiali



Turbina Centripeta



$$l_e = \frac{c_1^2 - c_2^2}{2} + \frac{u_1^2 - u_2^2}{2} - \frac{w_1^2 - w_2^2}{2}$$

$$u_1 > u_2$$



Turbina Ljungstrom

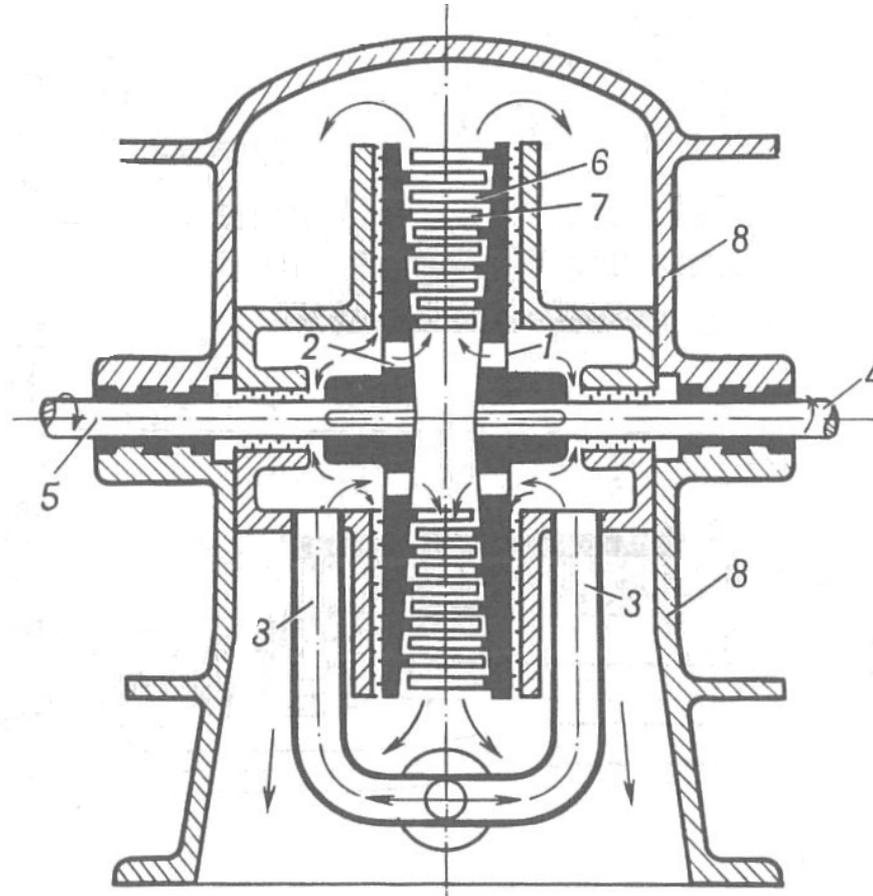
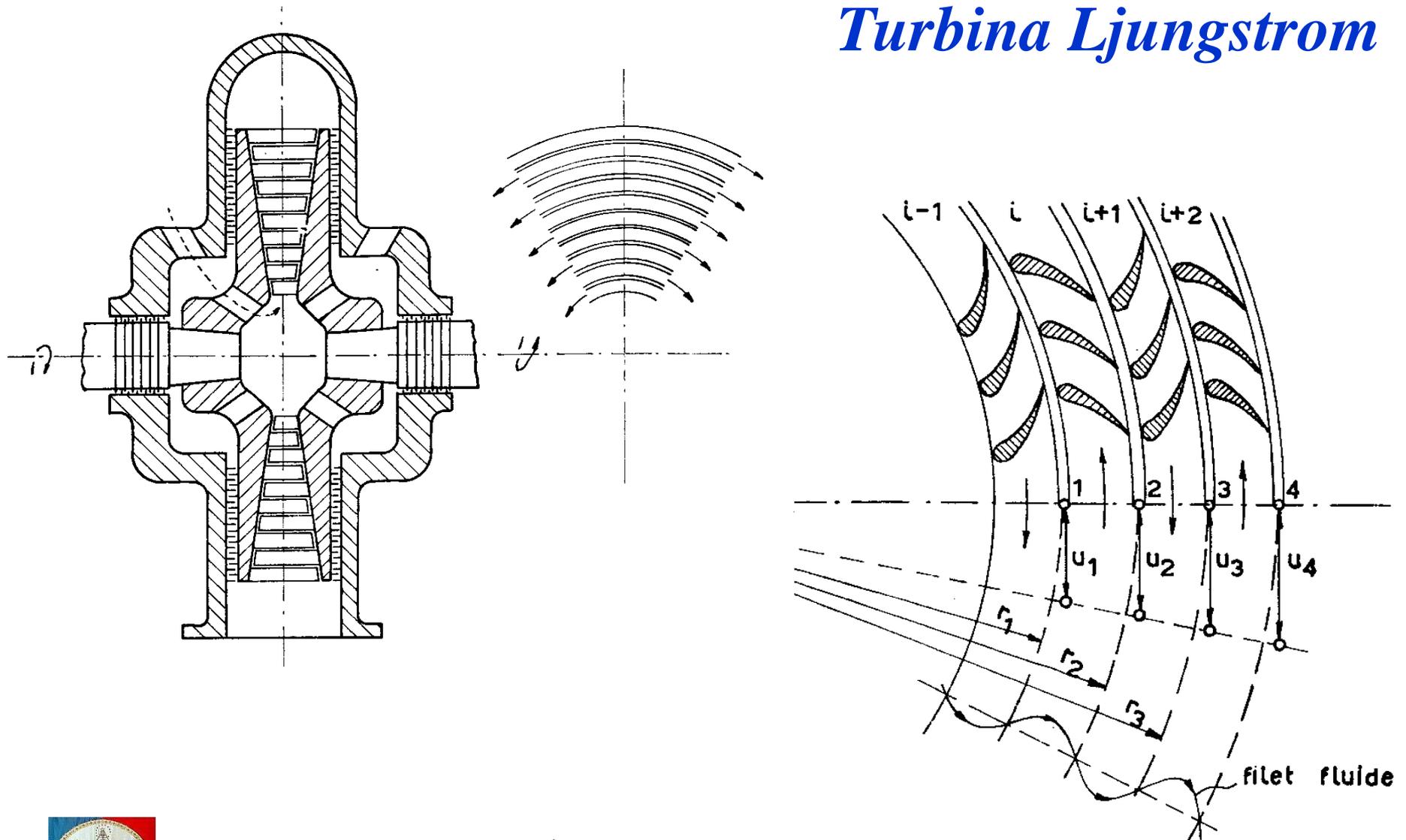


Fig. 1-3. Dibujo esquemático de la turbina radial de rotación en sentido inverso (Ljunström).

1, 2, discos de la turbina; 3, conductos de vapor vivo; 4, 5, árboles de la turbina; 6, 7, paletas de los escalones intermedios; 8, cuerpo.



Turbina Ljungstrom



Turbina Ljungstrom

